# The Effect of Biodiesel Derived from Waste Oil on Engine Performance and Emission Characteristics

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Received: July 2, 2018	Accepted: July 25, 2018	Online Published: July 31, 2018
doi:10.20849/jess.v1i1.432	URL: https://doi.org/10.20849/jess.v1i	1.432

## Abstract

To produce biodiesel from waste oil and use it as an alternative fuel in compression ignition (CI) engines is an efficient way to eliminate this harmful compound. In this experimental study, the effects of biodiesel derived from waste oil on emission and performance characteristics of CI engine were investigated. The production of biodiesel was realized at the condition: 9wt% acid catalyst amount, 9:1 molar ratio,  $60^{\circ}$ C reaction temperature and 120min reaction time. Biodiesel and diesel were mixed with different volumetric ratios and the properties of each blend were analyzed. Each blend was tested with a direct injection CI engine to see the effect of biodiesel on performance comparing to diesel. The use of biodiesel derived from waste oil led to decrease in hydrocarbon (HC), carbon monoxide (CO) emissions and smoke opacity up to 81.25%, 55.02% and 40.48% respectively while led to slight increase in nitrogen oxides (NO<sub>x</sub>) emissions in general.

Keywords: biodiesel, diesel engine, exhaust emissions, waste oil

## 1. Introduction

Fossil-based fuels used in the production of energy release a large share of pollutant emissions into the environment. The pollutant emissions, especially CO, HC,  $NO_x$  and PM, cause regional air pollution that threaten people health and environment worldwide (Sanjid et al., 2014). They have also contributed to the enhancement of the natural greenhouse effect led to climate change. Because of their high proportion in releasing pollutant emissions, fossil-based fuels are considered as the main reason of global climate change (Resitoglu et al., 2015).

Use of alternative sources instead of fossil-based fuels has been a common application by researchers to prevent the damage of fossil-based fuels. In researches carried on alternative sources, the use of local, renewable and clean sources, the increase of productivity and ensuring diversity of sources are the main factors that have been considered. The alternative sources met these factors may be listed as solar, wind, hydro, nuclear and biomass energy. Among these alternative energy sources, biomass energy has so many advantages to be alternative for fossil-based fuels. Biodiesel as one of the biomass-based fuels is an alternative and renewable source for fossil-based diesel (Qi et al., 2016; Ahmed et al., 2014).

The high production cost of biodiesel depend on raw material is the main obstacle in biodiesel's widespread use by comparison with diesel. In order to decrease the cost of biodiesel, waste oils that are easily available have become resources for biodiesel production (Qi et al., 2016). The use of waste oils instead of high cost vegetable oil in production of biodiesel is an effective way to reduce raw material costs (Eguchi et al., 2015). It is estimated that the use of waste oils instead of vegetable oils can reduce biodiesel production costs by 60-90% (Kochepka et al., 2015). In addition, using waste oils may also help to solve the problem of waste oil disposal.

Low cost feedstocks such as used cooking oils and animal fats are important sources for biodiesel production (Chuah et al., 2016). Many investigations have been carried out using biodiesel produced from waste oils in diesel engines. In these investigations, including waste cooking oils first, many waste oils from different origins

such as frying, fish, chicken, palm, coffee, limed fleshing, plastics, etc. have been used (Eguchi et al., 2015; Gürü et al., 2010; Chuah et al., 2016). Unlike these feedstocks, waste oil originated from kitchens, restaurants or refectories is an alternative feedstock in biodiesel production.

This experimental study aimed to demonstrate that this feedstock could be used as an alternative fuel in diesel engines. In this purpose, biodiesel production from waste oil was realized with esterification method. Blends of biodiesel and diesel were prepared in different volumetric ratios and fuelled CI engine to see the effects on diesel engine characteristics.

## 2. Material and Methods

Waste oil contained higher levels of free fatty acids was obtained from Çukurova University refectory's sewerage system. The waste oil was mixture of oil, water, solids and fats. It was obtained from this system is averagely 200L per week. Six different samples of waste oil used in biodiesel production were obtained at different times. All samples were mixed and specifications of composition were identified. The density, viscosity and free fatty acid values of composition were obtained as 909kg/m<sup>3</sup>, 28.7mm<sup>2</sup>/s and 65.15% respectively. Because of these high rates, esterification method was used for biodiesel production.

Biodiesel production from waste oil was carried out optimally with 9wt% acid catalyst amount and mol. ratio of 9:1, at reaction temperature of 60°C and reaction time of 120min. Methanol and sulphuric acid were used as alcohol and catalyst respectively. The flow diagram of the biodiesel production from waste oil is given in Figure 1. As shown in figure, after filtering, washing and drying processes, waste oil was subjected to esterification reaction with sulphuric acid and methanol. After the esterification reaction, water and catalyst were separated and crude biodiesel was washed and dried, in order to obtainment of pure biodiesel.



Figure 1. Flow diagram of biodiesel production from waste oil

Biodiesel produced from waste oil was mixed with diesel by volumetric rate of 10%, 20%, 30% and 40%. Each blend was named according to biodiesel rates (B10, B20, B30 and B40). Chemical and physical properties of blends were analyzed at Fuel Analysis Laboratory of Cukurova University. The equipments used for analyzing specifications of test fuels are given in our previous study (Keskin et al., 2015).

The physical and chemical properties of biodiesel and its blends with diesel are presented in Table 1. Biodiesel, diesel and diesel-biodiesel blends specifications have been determined according to EN 14214 Standards. The viscosity of pure biodiesel was found higher than that of diesel and standards. The lower heating value (LHV) decreased with use of biodiesel. Compared to diesel, biodiesel has a lower LHV at a rate of 12.97%. The LHV of blends decreased depending on increase rate of biodiesel content in the blend. The reduction rates in LHV of B10, B20, B30 and B40 were obtained as 1.56%, 3.23%, 4.99% and 6.70% respectively. The flash point of biodiesel is higher than that of diesel. The high flash point of biodiesel makes its storage and transportation easy and possible (Shadid & Jamal, 2008).

Quality	Unit	B10	B20	B30	B40	Biodiesel	Diesel	EN14214	EN590
Density	kg/m <sup>3</sup>	836	843	850	856	896	829	860-900	820-860
Viscosity (40°C)	mm <sup>2</sup> /s	2.4	3.2	3.91	4.78	9.88	2	3.5-5.0	2.0-4.5
Acid value	mgKOH/g	0.27	0.48	1.07	1.58	3.92	0.05	Max. 0.5	-
Flash point	°C	63.5	64.5	65.4	66.5	96.8	62.5	Min. 101	Min 55
Sulfur content	wt%	0.0813	0.0770	0.0706	0.0672	0.0538	0.0826	0.001	Max 0.2
Copper strip corrosion	-	1a	1a	1a	1a	la	1a		1
Lower heating value	kJ/kg	44016	43271	42485	41719	38913	44717		-

Table 1. Physical and chemical properties of test fuels

Table 2. Technical specifications of test engine

Model of engine	Antor Diesel 4 LD 640		
Number of cylinder	1		
Displacement	638cm <sup>3</sup>		
Bore x Stroke	95mm x 90mm		
Compression ratio	17:1		
Max. speed	3000min <sup>-1</sup>		
Max. power	10kW		
Max. torque	43Nm (1800min <sup>-1</sup> )		
Injection system	Direct injection		
Method of cooling	Air-cooled		

An air-cooled direct-injection single-cylinder Lombardini 4LD 640 CI engine was used at the performance and emission tests. Table 2 indicates the specifications of test engine. The smoke opacity values (K) of biodiesel, diesel and diesel-biodiesel blends were analyzed with CAP 3200 gas analyzer and Testo 350-S gas analyzer was used to measure HC, NO<sub>x</sub> and CO emissions. Details of these equipments are shown in Table 3. Schematic view of experimental set-up is given in Figure 2. The test engine was mounted on a platform and probes of gas analyzers were connected to the exhaust outlet line. A hydraulic dynamometer was used to install load to engine. The experimental uncertainties are given in Table 4.

Table 3	. The	main	properties	and	resolution	of	the ga	s analyz	zers
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Equipment		Range of measurement	Stability
	NO <sub>x</sub>	0-3000ppm	1
Testo 350-S	НС	0-20000ppm	1
	CO	0-10000ppm	1
CAPELEC CAP3200	K value	0-10L/m	0,01



Figure 2. Schematic figure of test rig (1. Control board, 2. Hydraulic-dynamometre, 3. Loading unit, 4.Rev-meter, 5. Platform, 6. Diesel engine, 7. Smoke meter, 8. Fuel tank, 9. Diesel emission analyzer)

Table 4. Uncertainties in	measurements
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Measurements		Uncertainty ±%
Power	kW	0.32
Torque	Nm	0.29
BSFC	g/kWh	0.97
Engine speed	min <sup>-1</sup>	0.13
Smoke	$m^{-1}$	2.27
СО	ppm	2.36
нс	ppm	1.93
NO <sub>x</sub>	ppm	2.76

The engine was run for 20min before the tests to reach active temperature of engine. To determine the emission and performance characteristics of test fuels, engine was removed to the maximum speed that it could be reached and the hydraulic dynamometer was started to load. Tests were carried out from 1200 to 2600rpm engine speeds at full load conditions. Each test was implemented for three times and the average of readings was counted. The engine power, torque and break specific fuel consumption (BSFC) were measured at the engine performance tests while CO,  $NO_x$ , HC and smoke opacity were determined at the engine emissions tests.

### 3. Results and Discussion

### 3.1 Engine Performance

Figure 3 and Figure 4 show engine torque and power curves respectively at full load condition and different engine speeds. As shown in the figures, despite the slight decrease in engine power and torque, it can be said that the engine power and torque characteristics of blends are similar to pure diesel. At all engine speeds, the engine power and torque decreased depending on the increase rate of biodiesel content in the blend. The maximum decrease in power and torque was obtained as 4.66% with B40 at 2600rpm compared to diesel. Averagely the decreases in power and torque were measured as 0.77%, 1.56%, 2.50% and 3.24% for B10, B20, B30 and B40 respectively. The lower LHV of biodiesel is the main reason for the decrease in engine power and torque. Besides, higher density and viscosity of biodiesel may cause flow problems that lead to lower combustion and thermal efficiency which decrease performance characteristics of diesel engine. Other investigators (Özsezen et al., 2009; Keskin et al., 2008) reported similar results.



The BSFC values of blends were higher than that of diesel in general (Figure 5). Compared to diesel, higher viscosity, lower LHV and higher density of blends led to increase in BSFC. The BSFC was reached the lowest value at 2400rpm with biodiesel, diesel and diesel-biodiesel blends while the highest BSFC values were measured at 1200rpm. Compared to diesel, the maximum increase in BSFC was obtained as 4.86% with B40 in 1800rpm. Considering all the engine speeds, B10, B20, B30 and B40 led to decrease in BSFC as a rate of 0.93%, 1.96%, 2.61% and 3.65% respectively. The BSFC reduction rates of blends were obtained parallel with the reductions rates in power and torque. Similar results were obtained in studies of other researches (Gürü et al., 2010; Kalligeros et al., 2003).



Figure 5. Break specific fuel consumption at full load condition

#### 3.2 Engine Emission Results

CO is a product formed due to incomplete combustion of fuels. Fossil-based fuels generate easily CO because there is not any oxygen in their molecular structure (Resitoglu et al., 2015). As seen in Figure 6, lower CO emission values were obtained with all blends compared to diesel. The maximum decrease rate in CO emission was 55.02% with B40 in 1200rpm. The minimum CO emission value was measured as 314ppm at 2200rpm with B40. Averagely the decreases in CO emissions were obtained as 30.70%, 36.17%, 37.73% and 41.45% for B10, B20, B30 and B40 respectively. The main reason of decrease in CO emission with blends is the oxygen content in the biodiesel, which increases air/fuel ratio especially at rich regions in terms of fuel and helps for the complete combustion (Qi et al., 2010).



The HC emission variations for different blends and diesel fuel are indicated in Figure 7. HC emission values decreased with all blends compared to diesel. The maximum HC emission values were measured at 1200rpm for all test fuels. Especially, HC emissions values were obtained higher in low engine speed due to low inlet airflow that affects turbulence and homogeneity of air-fuel mixture in the cylinder. The HC concentrations at 1800rpm (speed at maximum engine torque) was decreased by 30.06%, 40.13%, 45.03% and 55.11% with use of B10, B20, B30 and B40 respectively comparing with diesel. These results show that HC emissions reduced significantly with use of biodiesel. The reduction of HC emissions could be explained with the complete combustion of the fuel droplets.



Figure 7. HC emissions at full load condition

 $NO_x$  emission values of test fuels are given in Figure 8. As shown in figure,  $NO_x$  concentration was increased in direct proportions with increases in percentage of biodiesel.  $NO_x$  emissions between 1400 and 1800rpm engine speeds were obtained higher than those at other engine speeds for all test fuels. Especially,  $NO_x$  emission values increased to the highest level near the engine speeds at which maximum torque was obtained. In the continuation of these speeds,  $NO_x$  emission was decreased with increase in engine speed because of shorter residence time available for formation of  $NO_x$ . Use of biodiesel led to increase in  $NO_x$  emissions averagely 8.72% for B10, 11.12% for B20, 12.55% for B30, 17.64% for B40. Other researchers obtained similar increases in  $NO_x$  emissions with use of biodiesel (Lapuerta et al., 2008; Lin et al., 2009). It is estimated that the increase in  $NO_x$  emissions depends on high temperatures of combustion meaning improvement of combustion with use of biodiesel.



Figure 8. NO<sub>x</sub> emissions at full load condition

Figure 9 shows smoke opacity values of the test fuels at full load condition. The smoke is formed due to incomplete combustion and denoted by the ratio of light absorb coefficient (K) (Qi et al., 2010). Compared to diesel fuel, smoke opacity values of blends decreased at all engine speeds. The minimum smoke opacity value was measured as 0.25L/m at 2000rpm with B40. The smoke opacity values were higher at high and low engine speeds compared to medium engine speeds. Maximum reduction in smoke opacity was obtained as 40.48% with B40 at 2000rpm. Smoke opacity values decreased averagely 7.80% with B10, 10.77% with B20, 14.68% with B30 and 20.19% with B40.



# 4. Conclusion

This paper focused on production biodiesel from waste oil and use as an alternative fuel in CI engines. Waste oil contained high rate of free fatty acid was obtained from a refectory's oil separator and esterified to get biodiesel. Brief engine tests were conducted using different combinations of biodiesel and diesel fuel. In conclusion, the engine torque and power decreased slightly while BSFC increased in direct proportions with increases in percentage of biodiesel. Maximum increase in BSFC was obtained as 4.86% with B40 at 1800rpm.

The use of biodiesel derived from waste oil as a blend fuel in diesel engine improved the emission characteristics. Compared to diesel, significant reductions were detected in CO and HC emissions with blended fuels while  $NO_x$  concentration increased slightly. Maximum decreases in CO and HC emissions were obtained with B40 respectively as 55.02% at 1200rpm and 81.25% at 2000rpm. Use of biodiesel led to decrease up to 40.48% in smoke opacity. Finally, this study indicated that the biodiesel produced from waste oil could be used in diesel engine. The use of waste oil as an alternative fuel has a positive impact upon ecological and economic sense.

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